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June 22, 1965

## LINEAR PHASOLVER MEASURING ENGINE

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and line	g the measuring engine is a difficult proposition ar measuring is tougher than retary measuring of scale factor variations.	
Phasolve fraction by measu	the test data seems to indicate that the Lines: or electronics and patterns can measure to a of 1/10 micron is trying to prove it ring gage block lengths. The variables they must with are:	STAT
a)	Manual dexterity of the physical arrangement. The principal precaution is to not tilt the gage block and thus not measure a false length.	
b)	Variations in null position of microinch mater. Over short periods, this appears to be accurate to a few micro inches.	STAT
c)	Thermal variations in gage block lengths. They have obtained additional gage blocks to make a complete set for measuring 1/8 mm increments within the 1 mm pole pair length in addition to the five lengths of 23 mm, 30 mm, 60 mm, 125 mm, and 250 mm. Thus handling and thermal problems are decreased.	
d)	Temperature and humidity effects on other com- ponents. Room temperature is continuously recorded and is within 1°F. Humidity is con- tinuously recorded and is within about 3%.	
of	the Phasolver technique of measuring and the linear phasolver feasibility model. The	STAT
inspecte	ad the linear phasolver feasibility model. The representatives were:	STAT

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He began the day highly skeptical of the practicability of the phasolver approach, particularly the electronics. was able to demonstrate better than 1/10 micron STAT resolution and better than 1/2 micron peak to peak repeatability. By the end of the day, STAT the following reservations: A laser interferometer by its geometry appeared to be easier to incorporate into a measuring machine than the phasolver. STAT for t The phasolver cost of **b**) 2-axls system was high. In principle, a laser interferometer is much simpler and should be more accurate than the phasolver. The scale error in the present phasolver feastbility model would not meet his requirements. STAT and the others seemed to be On the other hand convinced that: The linear phasolver did produce a unique, una) ambiguous measurement of position. There was no limitation on slewing rate from one measuring point to enother. The velocity error was probably satisfactory for servo drive of a slaved platen to retain stereo registration while moving. Repeatability accuracy was 1/2 micron peak to d) peak or better. One additional point that came out of the meeting had to do with skew and tilt of the phasolver plates. Part of the test program calls for measurement of the STAT sensitivity of phasolver accuracy to relative skew of the driver and coupler plates and variations of the gap between the plates, including tilt. Indicated that the STAT guiding ways and air bearings on his machine would hold skew to only a few seconds of arc and variations in the gap to 100 microinches (2½ microns), peak to peak. These variations are so small that measuring their effect of the phasolver is of second order of importance. has now turned their attention to scale factor. STAT Scale factor error has two parts: a) error within a sine wave cycle pole pair (a pole pair is one millimeter long)

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and b) the incremental error from pole pair to pole pair

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over the 20 inch length. It should be noted that both these errors are systematic and can be corrected by computer computation.

Non-Linear scale error within a pole pair can be corrected by balancing the amplitude and quadrature of the driver pattern exciting voltages. The uncorrected non-linear error was 60 microns p-p. By balancing, this has been brought down to about 1.8 micron p-p including repeatability error. (Note this is later data than the previously reported 0.8 micron p-p scale error.) Further reduction is probably possible.

The scale error over 250 mm is about 13 microns with about a 3 micron curvature (i.e. non linearity). In discussion with their consultant from UCLA they decided that the resistance of the coupler pattern (which is about 2,000 chms) was probably introducing a phase shift as it varied from near zero when measuring at one end to its maximum value when measuring at the other end. Tests this week and last tend to confirm that the coupler pattern resistance is causing the 3 micron nonlinearity in the overall scale factor. The cause of the linear error in the scale factor has non been determined. measurement of the patterns indicates the scale ractor error should only be about microns whereas the test data indicate it is about 18 microns. Thermal expansion or contraction of the glass bar on which the coupler pattern is placed may be a factor. If the temperature of the glass ber at the time of making the pattern at and measuring the pattern at is different by about 6.70 from the temperature of the glass bar during the present test program, a scale factor error of the right magnitude could occur. Temperature difference is, however, probably only one contributor. accounting procedure has adjusted their man hour rates upward for the year due to increased overhead. This adjustment makes the contract over expended and they have officially stopped work. There is no estimate as to when they might resume work, if at all. The next phase of the phasolver program should, it seems to me, be a check of the effect of temperature and humidity and probably should be run under the direction of \_\_\_\_ to permit their thorough evaluation of the device. concurrance I discussed the possibility of running such a test in the clean room with

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